

Slow Slip and Dynamic Rupture as a Competition Between Dilatant Strengthening and Thermal Weakening

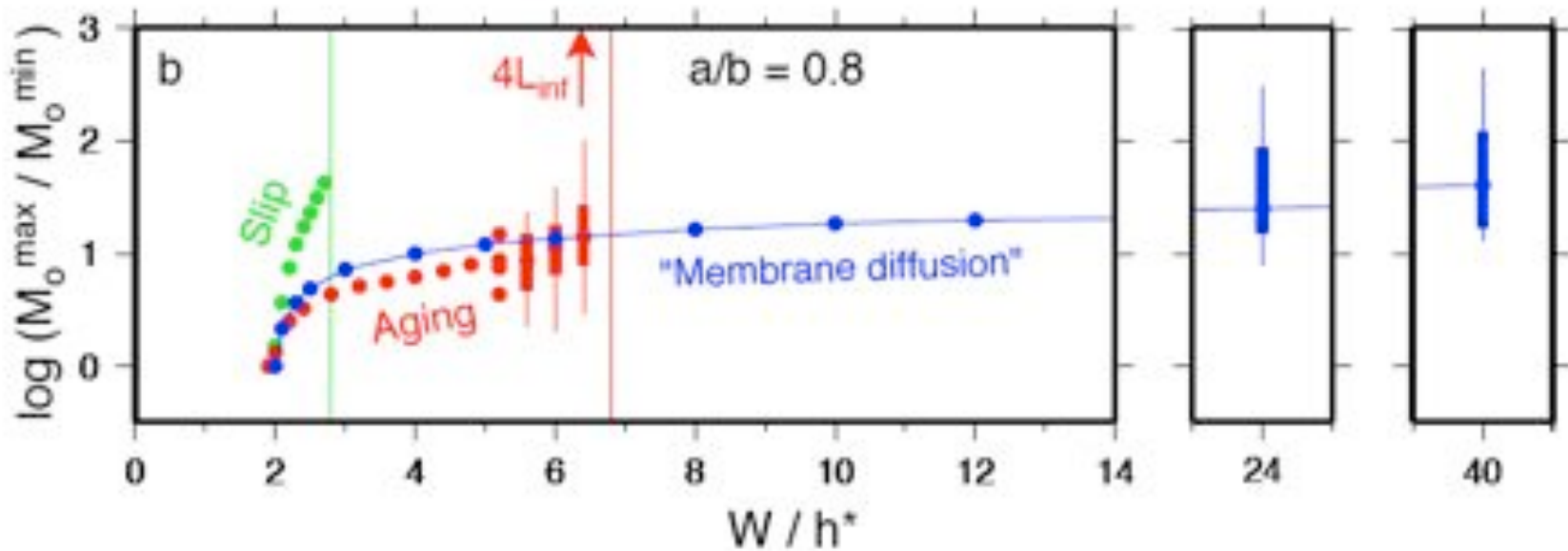
Paul Segall
Andrew Bradley
Stanford University

Also: Allan Rubin, Jim Rice, Yajing-Liu, and others

Possible Mechanisms for Slow Slip

- Change in frictional behavior at high slip speed [e.g., Shibazaki and Iio, 2003; Shibazaki and Shimamoto, 2007].
- Rate-state friction near neutral stability [Yoshida and Kato, 2003; Kuroki et al, 2004; Liu and Rice, 2005; 2007; Rubin, 2008].
- Stable friction perturbed from steady-state [Perfittini and Ampuero, 2009].
- Dilatant stabilization [Rice, 1975, Rice and Simons, 1976, Rudnicki, 1979]; in rate-state friction context [Segall and Rice, 1995; Segall and Rubin, 2007-9 AGU; Segall et al, 2010 in press, Liu and Rubin, in press], also Suzuki and Yamashita [2008, AGU; JGR, 2009].

Rate-State Friction Alone: Goldilocks Problem



Segall, Rubin, Bradley, Rice, JGR in press.

- Slip-zone too small -> No transient.
- Slip-zone too large -> Dynamic slip.
- "Just right" range small for preferred slip-law.
- Dilatancy removes this problem.

Hypothesis

Velocity weakening rate-state friction
nucleates localized slip.

If dilatancy stabilizes slip before thermal
weakening onset → slow slip.

If dilatancy unable to limit slip speeds below
thermal weakening limit → fast slip.

Previous work:

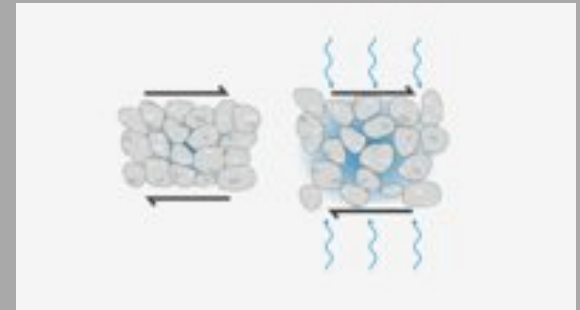
Isothermal approximate diffusion [Segall and Rubin,
2007 AGU; Liu et al 2008, AGU] building on Segall
and Rice [1995] and Taylor and Rice [1998].

Slip weakening, thermo-poro dynamic, short (10 s)
integration times [Suzuki and Yamashita, 2009; JGR]

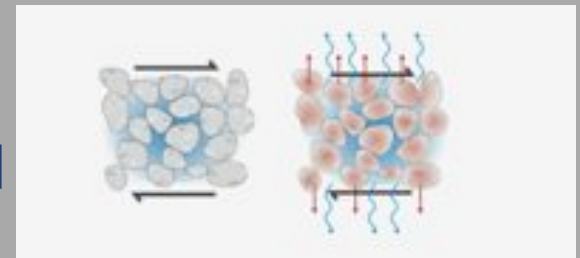
This work:

Rate-state proper thermo-poro diffusion, quasi-
dynamic, integrated over many cycles (centuries).

Dilatancy: stabilizing



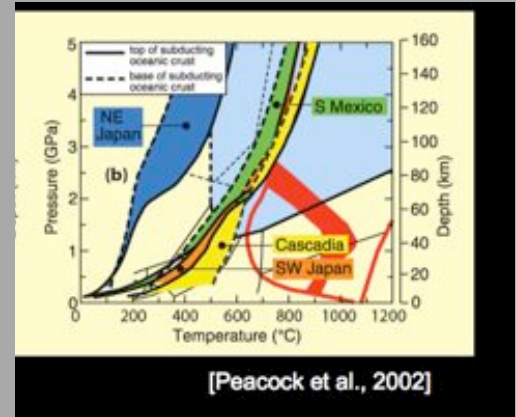
versus



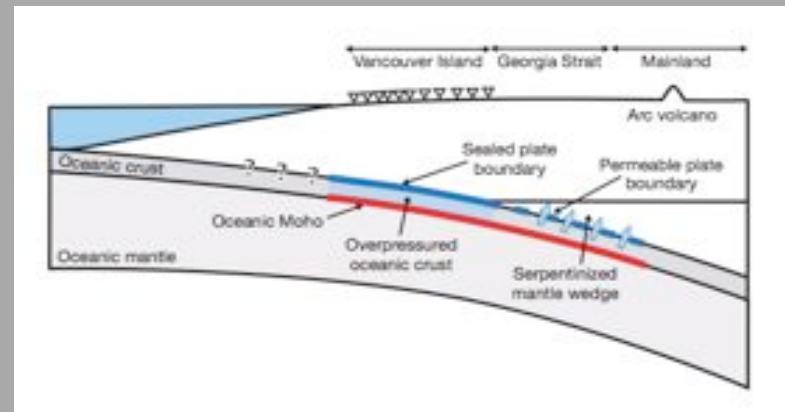
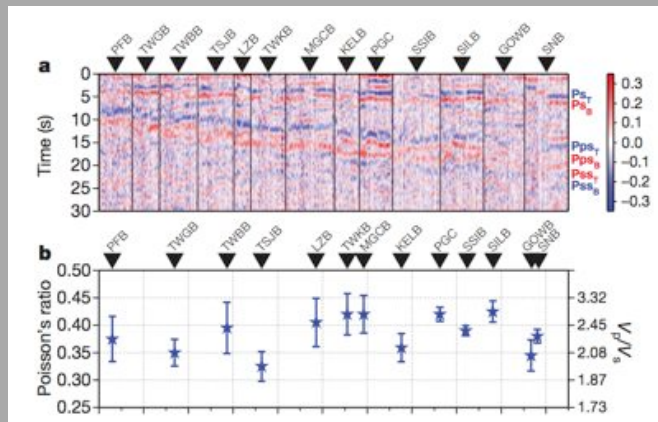
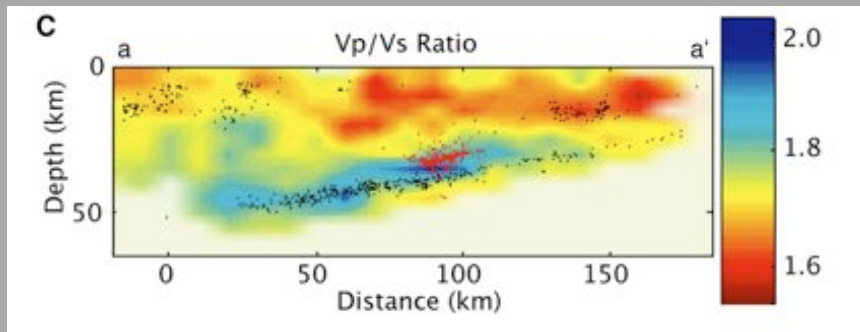
Thermal pressurization:
de-stabilizing

High Pore-Pressure in ETS zones

- High V_p/V_s
- Low Stress Drop
- Available Dehydration reactions



Shelly et al, 2006



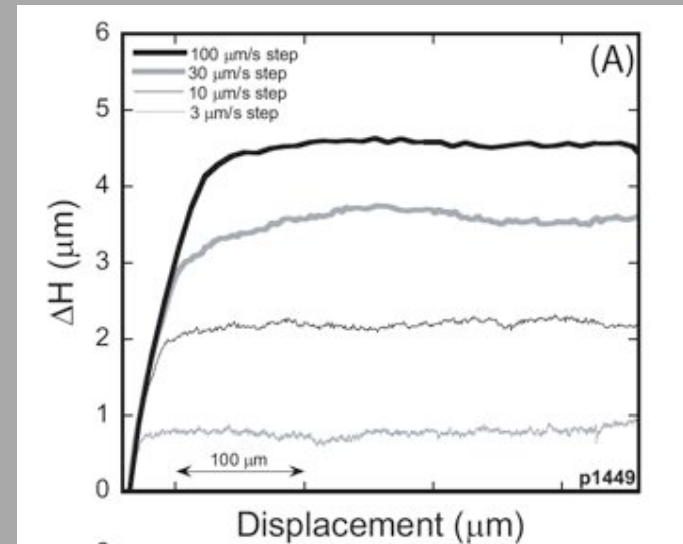
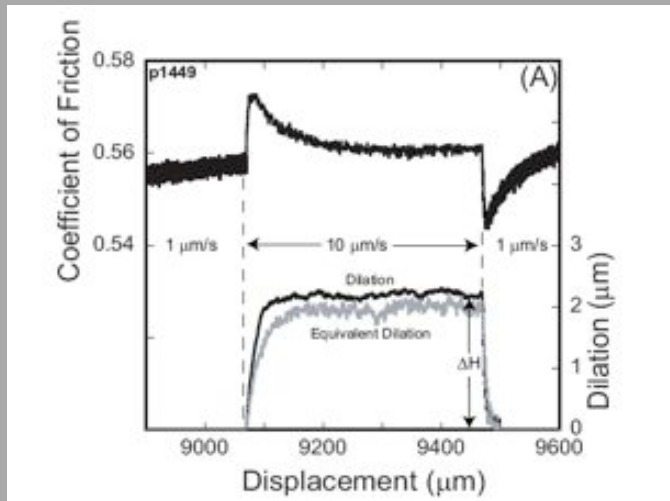
Audet et al, (Nature, 2009), conclude that near lithostatic pore-pressure in slab crust.

Thermal pressurization weak at low effective stress → stable slip.

Approach

- Include only well documented (if not fully understood) fault physics.
- To the extent possible, use physical parameters based on laboratory experiments and field observations.
- Employ efficient numerical methods that permit simulation of many slow-slip and earthquake cycles. Approximations:
 - 2 dimensional elasticity, 1D fault
 - Limit of very thin shear zone
 - Approximate elastodynamics
- Compare simulations with slow-slip observables.

Dilatancy/Compaction:



Samuelson, Elsworth, Marone, (2009)

Constitutive Law for Dilatancy: ϕ inelastic porosity, Segall and Rice [1995]

$$\frac{d\phi}{dt} = -\frac{v}{d_c} (\phi - \phi_{ss}) \quad \text{where} \quad \delta\phi_{ss} = \epsilon \log \left(\frac{v}{v_0} \right).$$

$\epsilon \sim 10^{-4}$, based on fits to Marone [1990] lab data.



Momentum Balance On Fault [e.g., Rice 1993]

$$\underbrace{\frac{\mu}{2\pi(1-\nu)} \int_{-\infty}^{\infty} \frac{\partial \delta / \partial \xi}{\xi - x} d\xi}_{\text{shear stress}} - \underbrace{f(v, \theta)(\sigma - p)}_{\text{frictional resistance}} = \underbrace{\frac{\mu}{2v_s} v}_{\text{radiation damping}}$$

μ : Shear Modulus, δ : Slip, f : friction coefficient, v : slip speed, θ : "state"

Rate state friction: Ruina [1983]; Dieterich [1979]; Linker and Dieterich [1992].

$$\tau = \underbrace{f(v, \theta)}_{\text{fric. coeff.}} \underbrace{(\sigma - p)}_{\text{effec. stress}} = (\sigma - p) \left[f_0 + a \ln \left(\frac{v}{v_0} \right) + b \ln \left(\frac{\theta}{\theta_0} \right) \right]$$

$$\frac{d\theta}{dt} = \underbrace{-\frac{\theta v}{d_c} \ln \left(\frac{\theta v}{d_c} \right)}_{\text{slip law}} - \underbrace{\frac{\alpha \theta}{b(\sigma - p)} \frac{d}{dt} (\sigma - p)}_{\text{Linker Dieterich effect}}$$

Fluid & Heat Transport for Thin Shear Zone

Heat & Pore-Fluid Transport for Thin ($h \rightarrow 0$) Shear Zone:

$$\frac{\partial T}{\partial t} = c_{th} \frac{\partial^2 T}{\partial y^2} \qquad \frac{\partial T}{\partial y} \Big|_{y=0} = -\frac{\tau V}{2\rho c_p c_{th}}$$

$$\frac{\partial p}{\partial t} = c_{hyd} \frac{\partial^2 p}{\partial y^2} + \underbrace{\Lambda \frac{\partial T}{\partial t}}_{\text{Shear Heating}} \qquad \frac{\partial p}{\partial y} \Big|_{y=0} = \frac{h\dot{\phi}}{2\beta c_{hyd}}$$

Thermal and hydraulic diffusivity, c_{th} , c_{hyd} , density, ρ , heat capacity, c_p thermal coupling parameter, $\Lambda = 1\text{MPa}/^\circ\text{C}$, fluid + pore compressibility, β .

[e.g., w/out dilatancy, Rice, 2006]

- Rate-State: $a/b < 1$, $f_0/b \simeq 30$, W/h^* fault width, where

$$h^* \equiv \frac{d_c \mu / (1 - \nu)}{(\sigma - p)(b - a)}$$

Nucleation dimension
(drained)

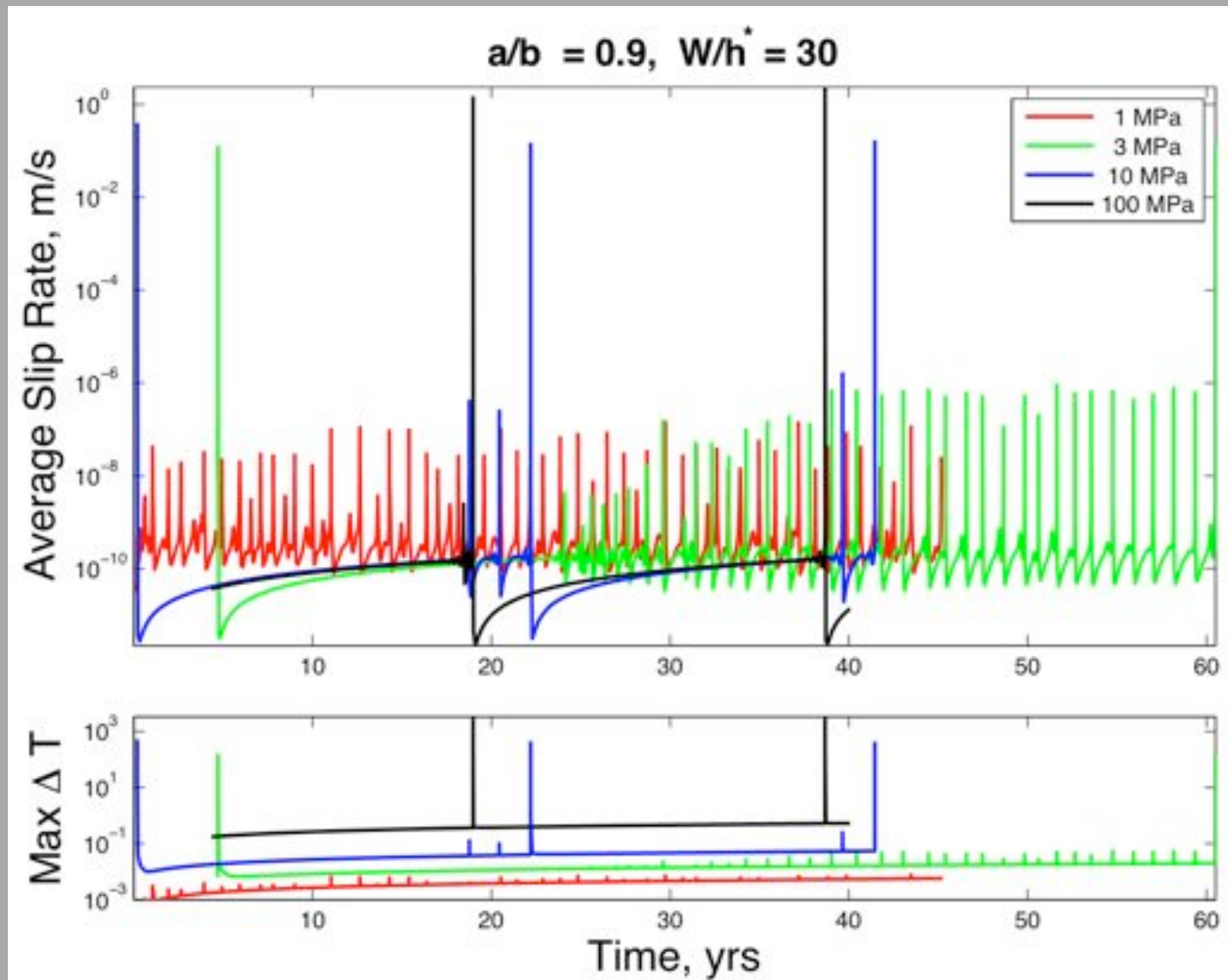
- Thermo-Poro: E_p , E_T , c_{th}/c_{hyd}
- Other: α/f_0 (Linker-Dieterich), $\mu v^\infty / 2b(\sigma - p^\infty) v_s \ll 1$ (radiation damping)

Dilatancy to Shear Heating Efficiency

$$\frac{E_p}{E_T} = \frac{\rho c_p}{f_0 \Lambda \beta (\sigma - p^\infty)} \left(\frac{\epsilon h}{d_c} \right) \left(\frac{c_{th}}{c_{hyd}} \right)$$

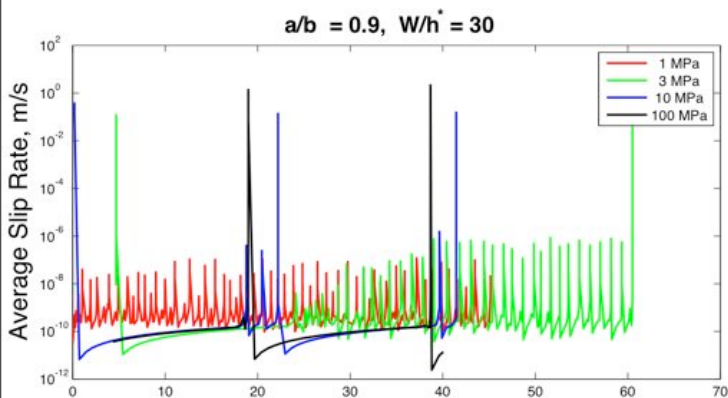
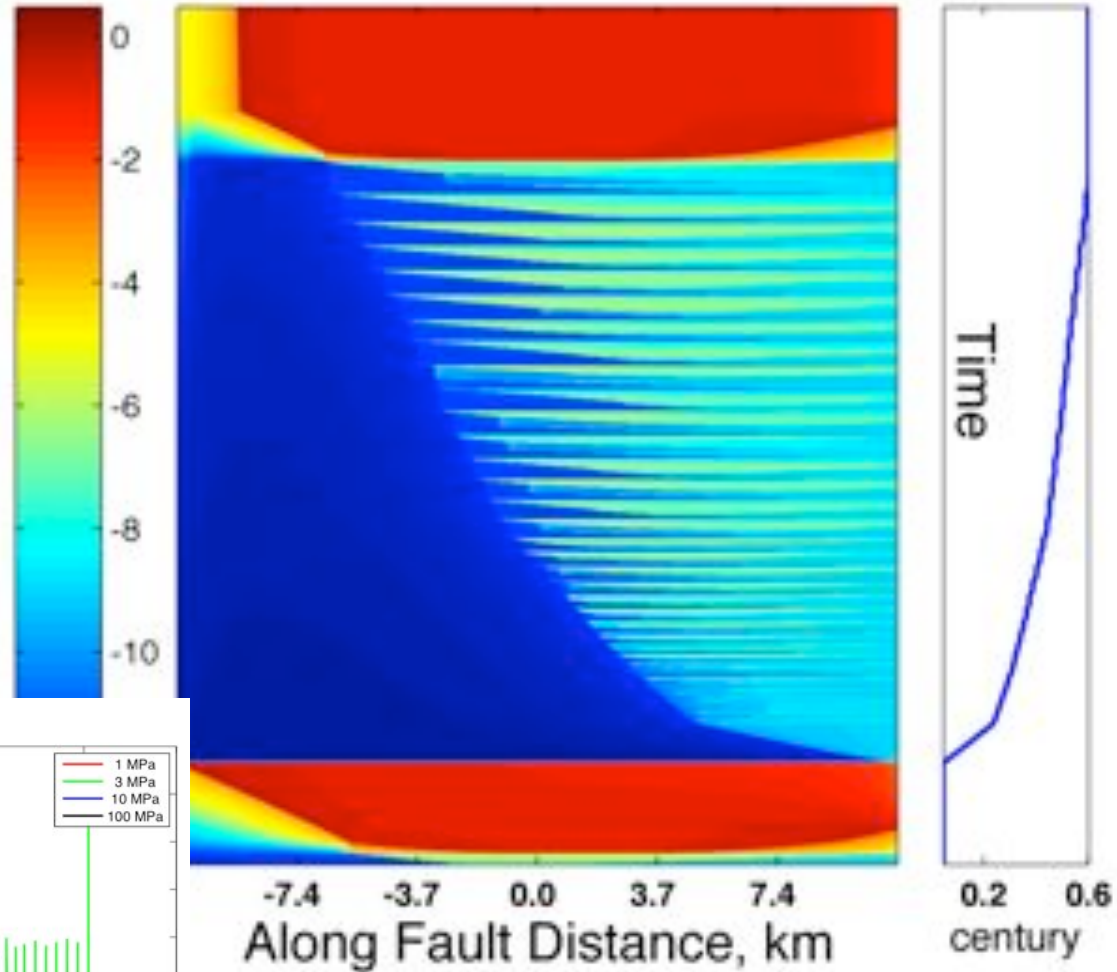
Low effective normal stress favors dilatancy → stable slip.

Stable at Low Effective Stress (Fixed Length)

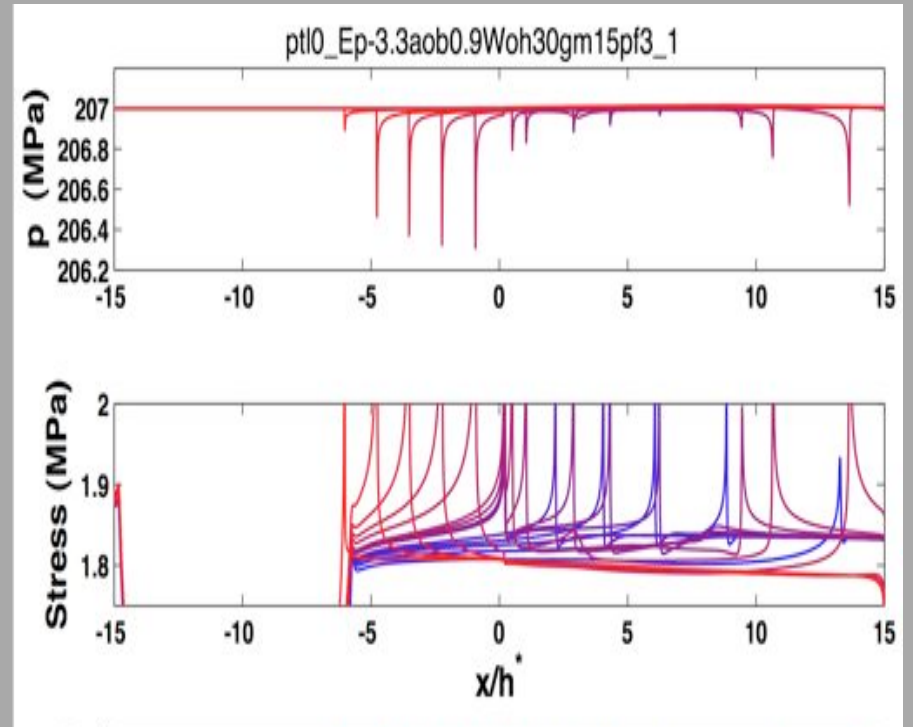
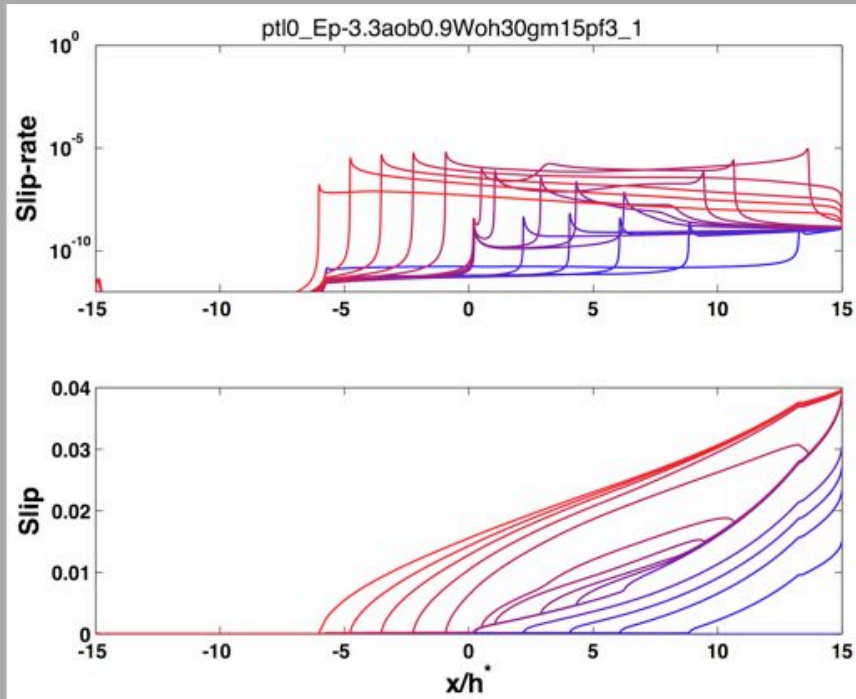


Space-Time Evolution: 3 MPa Effective Stress

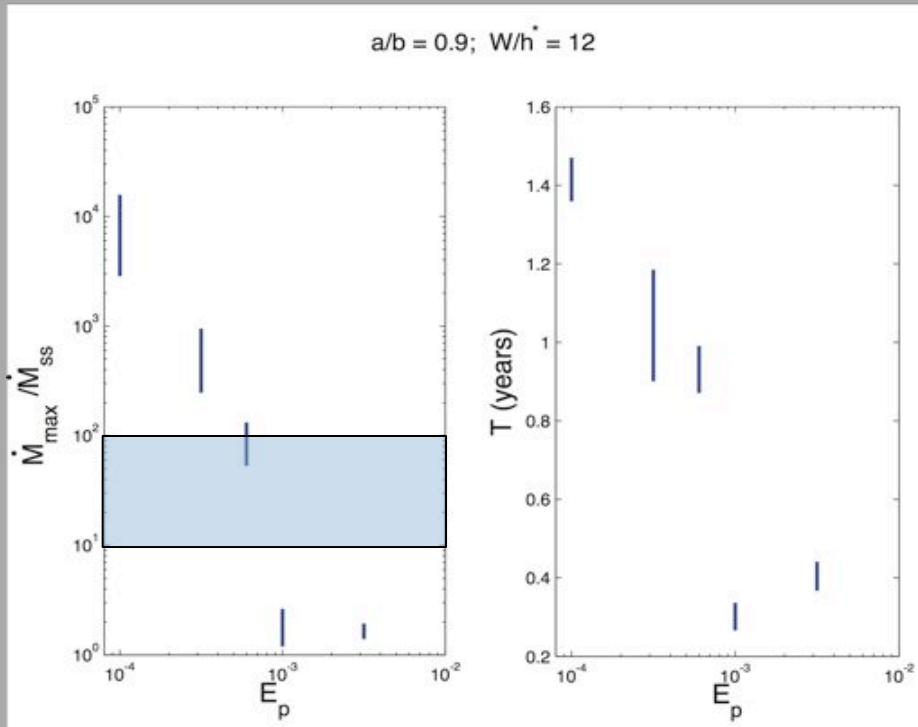
Log Slip-Rate: $\sigma = 3$ MPa; $a/b = 0.9$; $W/h^* = 30$



Slow Slip Phase: 3 MPa Effective Stress

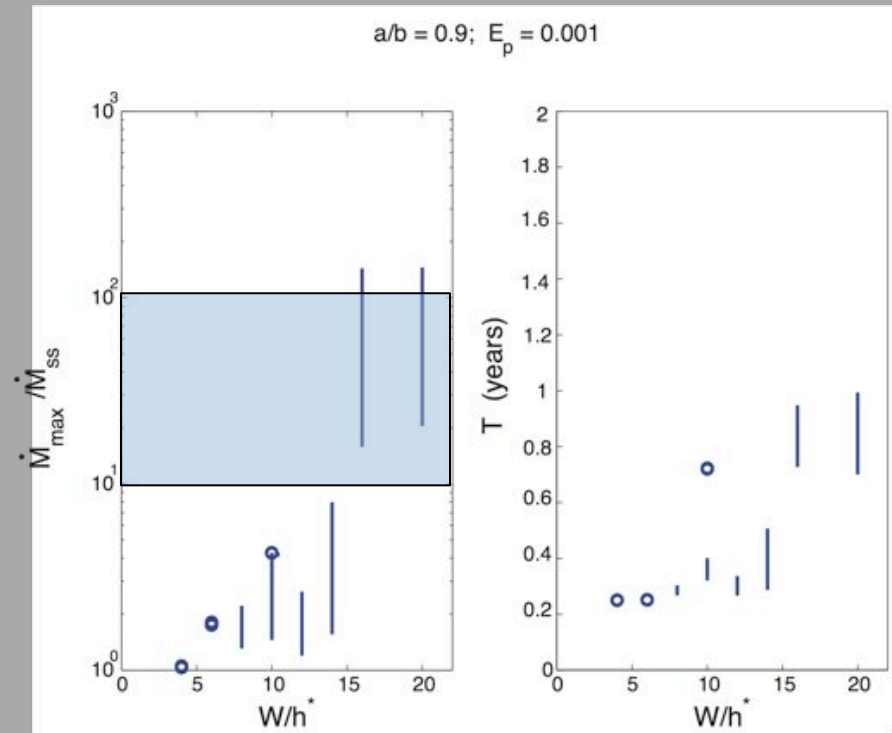


Slip Rate and Period in Range of Observations



→

Increasing Dilatancy or
Decreasing Eff. Stress

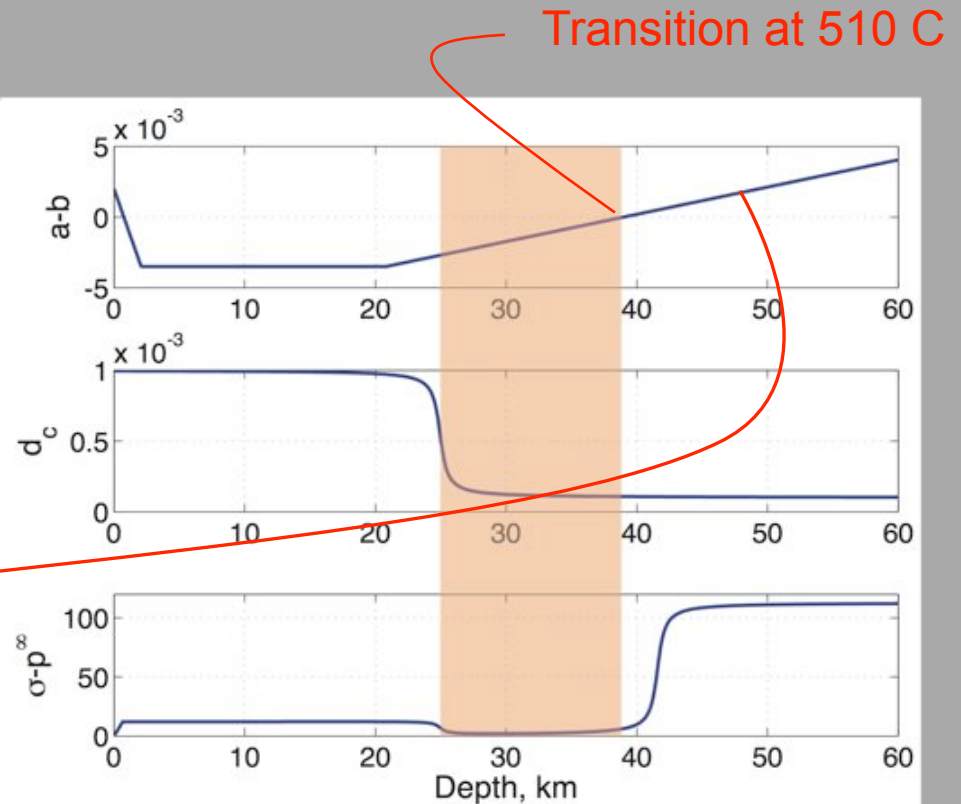
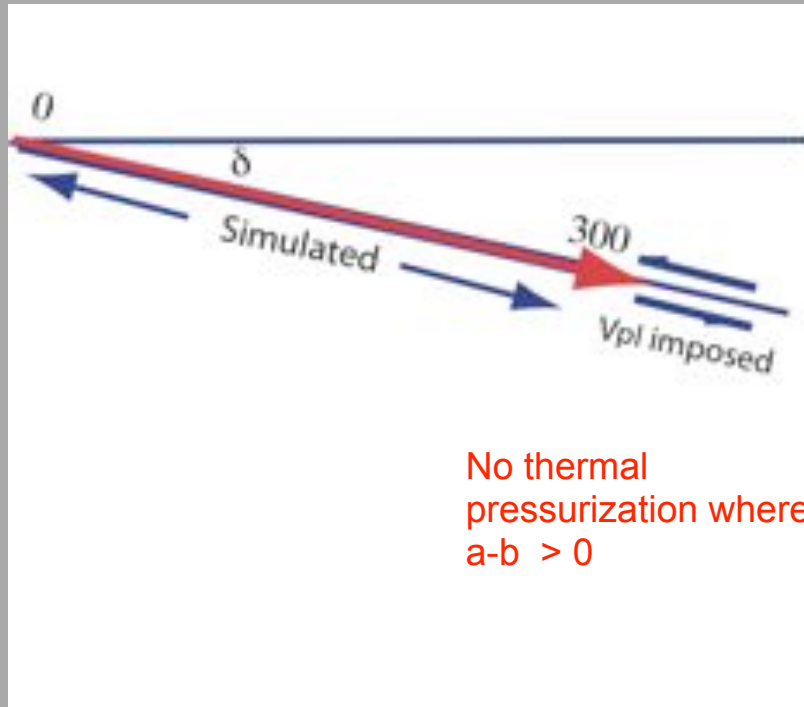


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Increasing Slip-zone Length

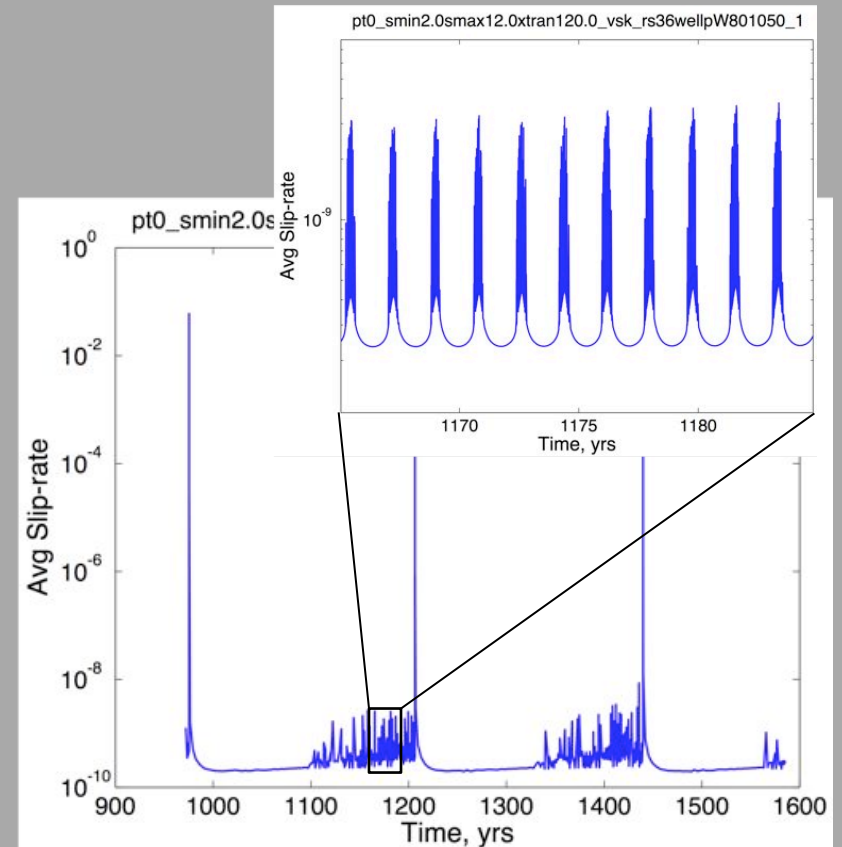
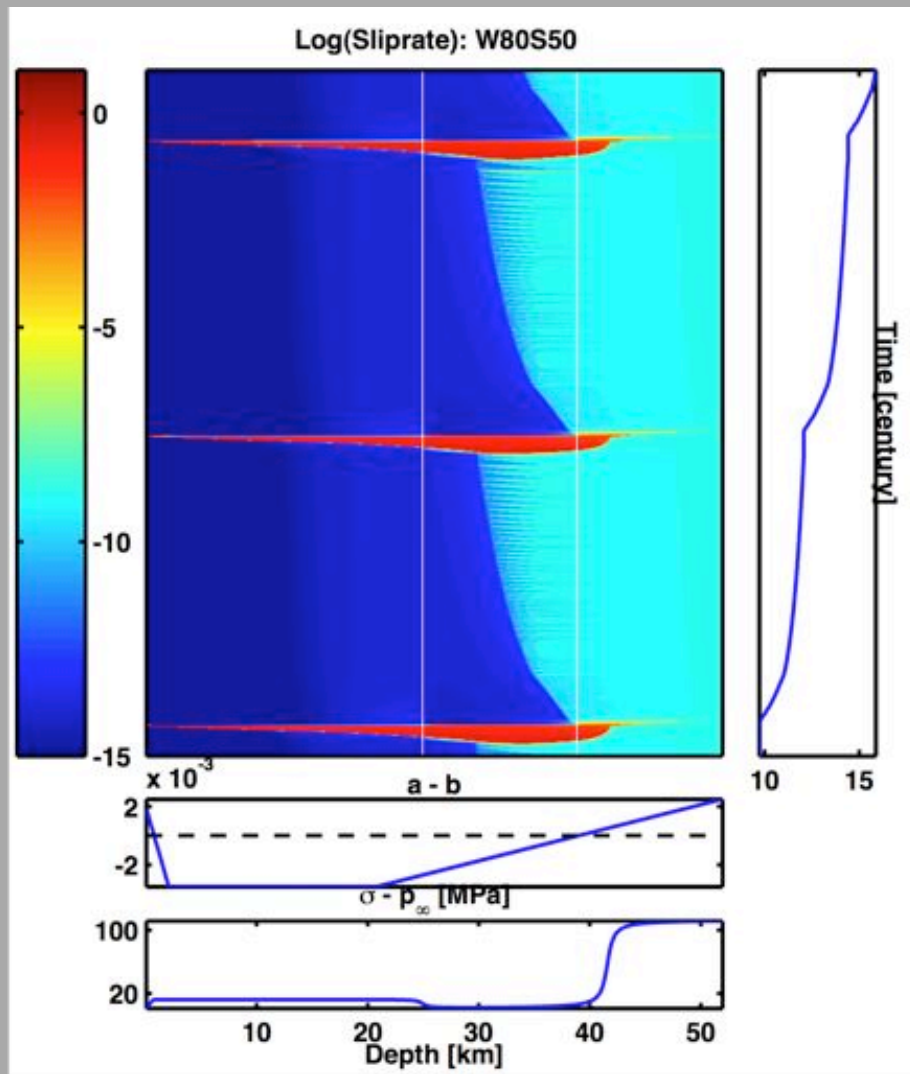
Slow-slip like behavior occurs for broad parameter range. (Isothermal calculations [Segall et al, 2010 in press])

Depth Dependent Properties and Effective Stress

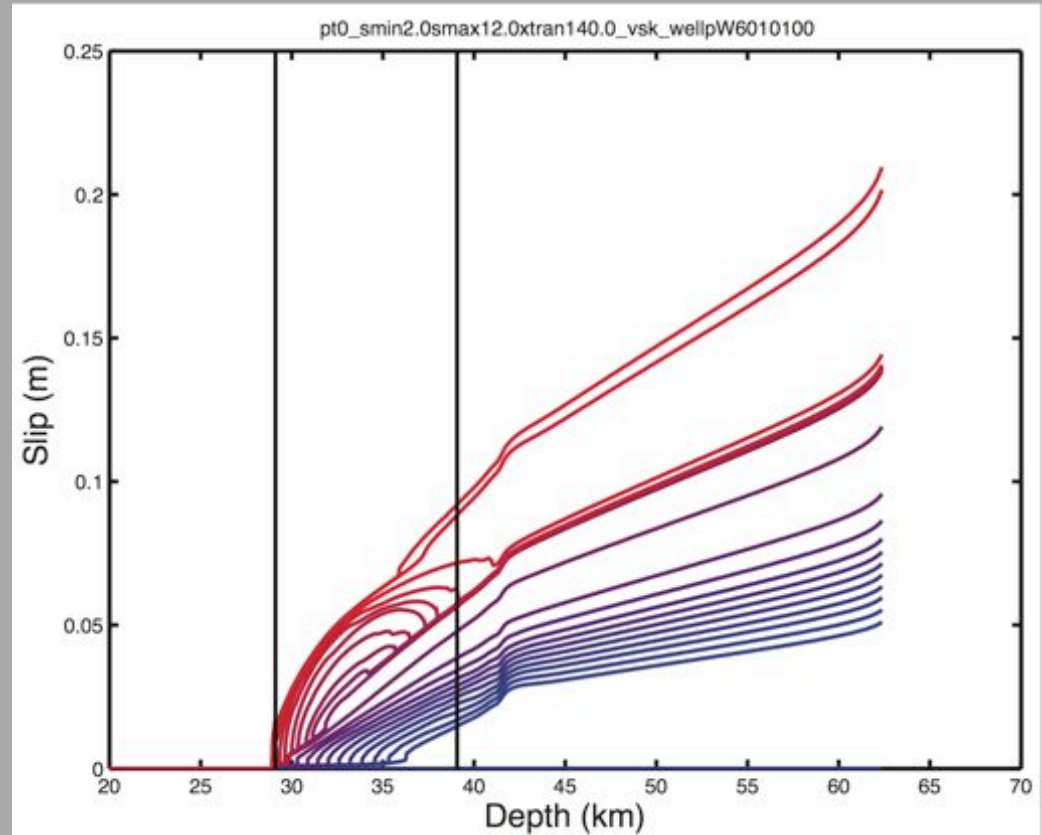
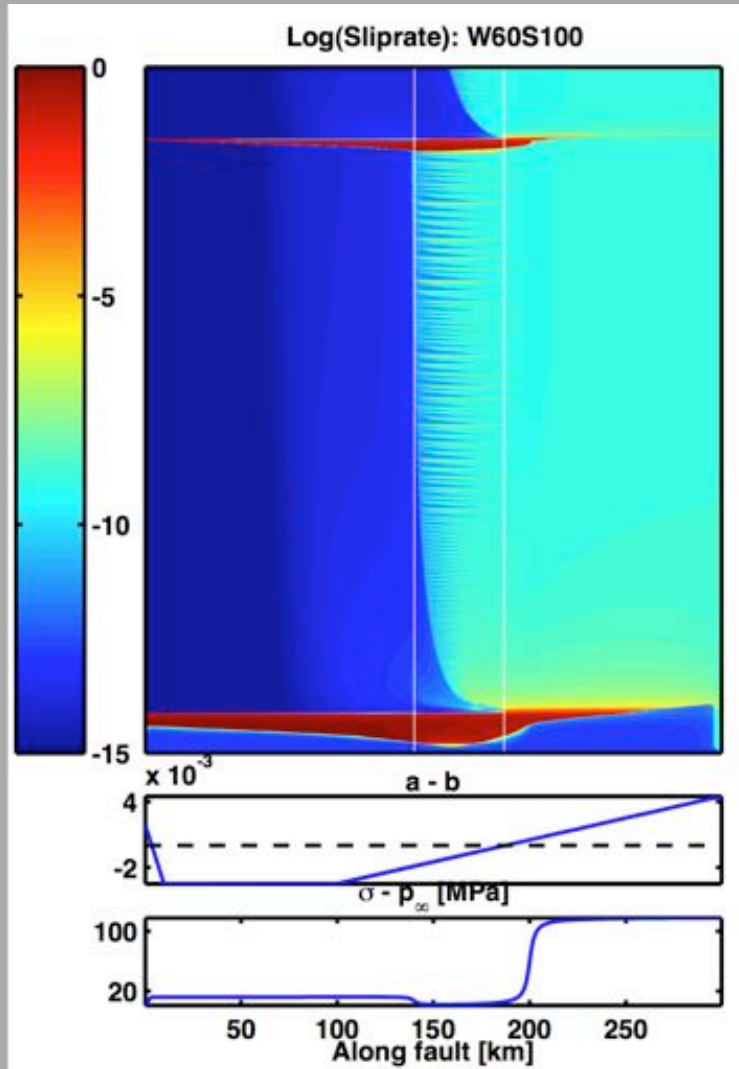


- Friction distribution loosely based on lab data for gabbro from He et al [2007], mapped to depth using Cascadia geotherm [Peacock, 2009], similar to Liu and Rice [2009].
- Very low effective stress in suggested ETS region, modest effective stress up-dip.

Slow slip events, occur spontaneously and may penetrate farther up-dip with time.

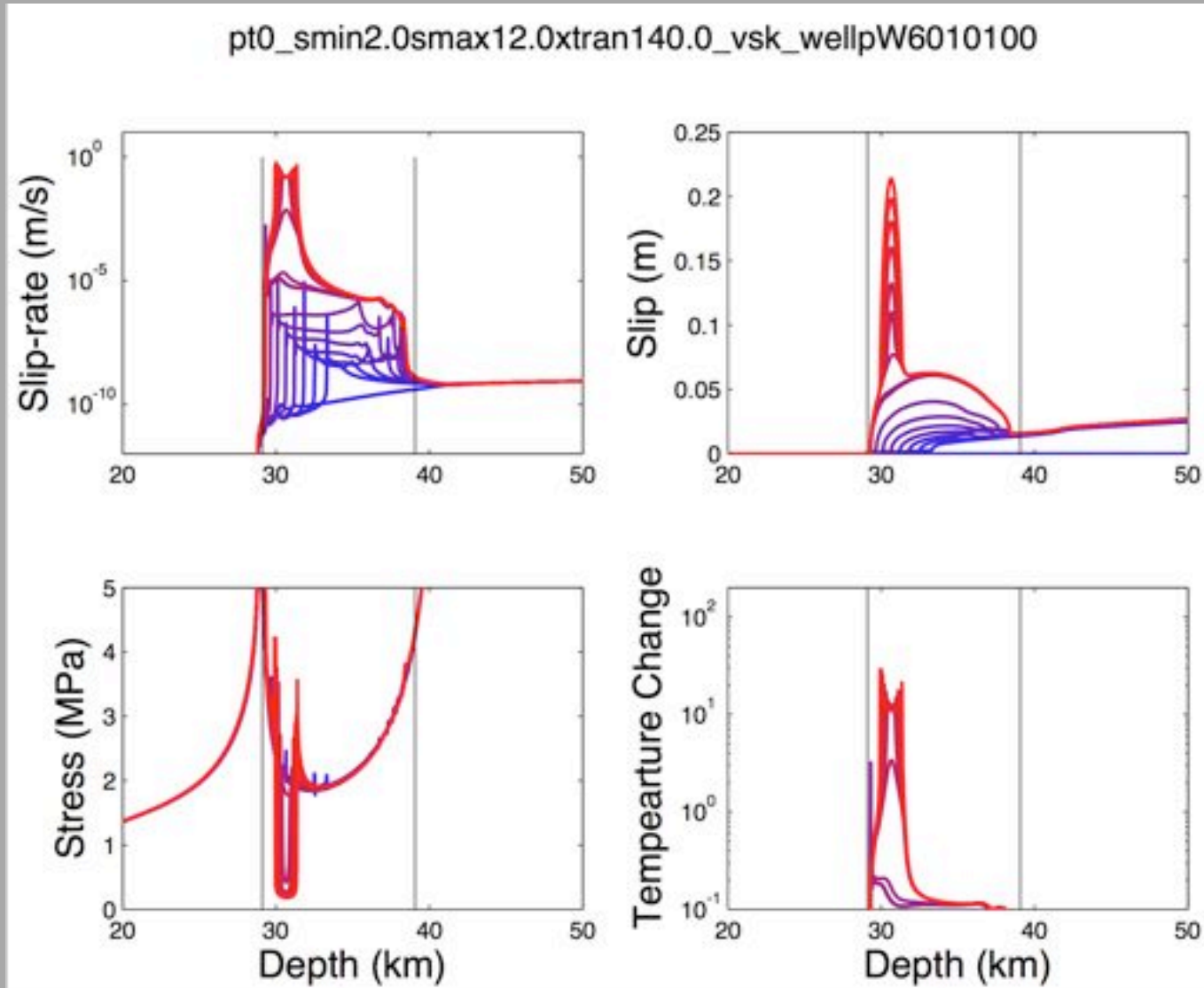


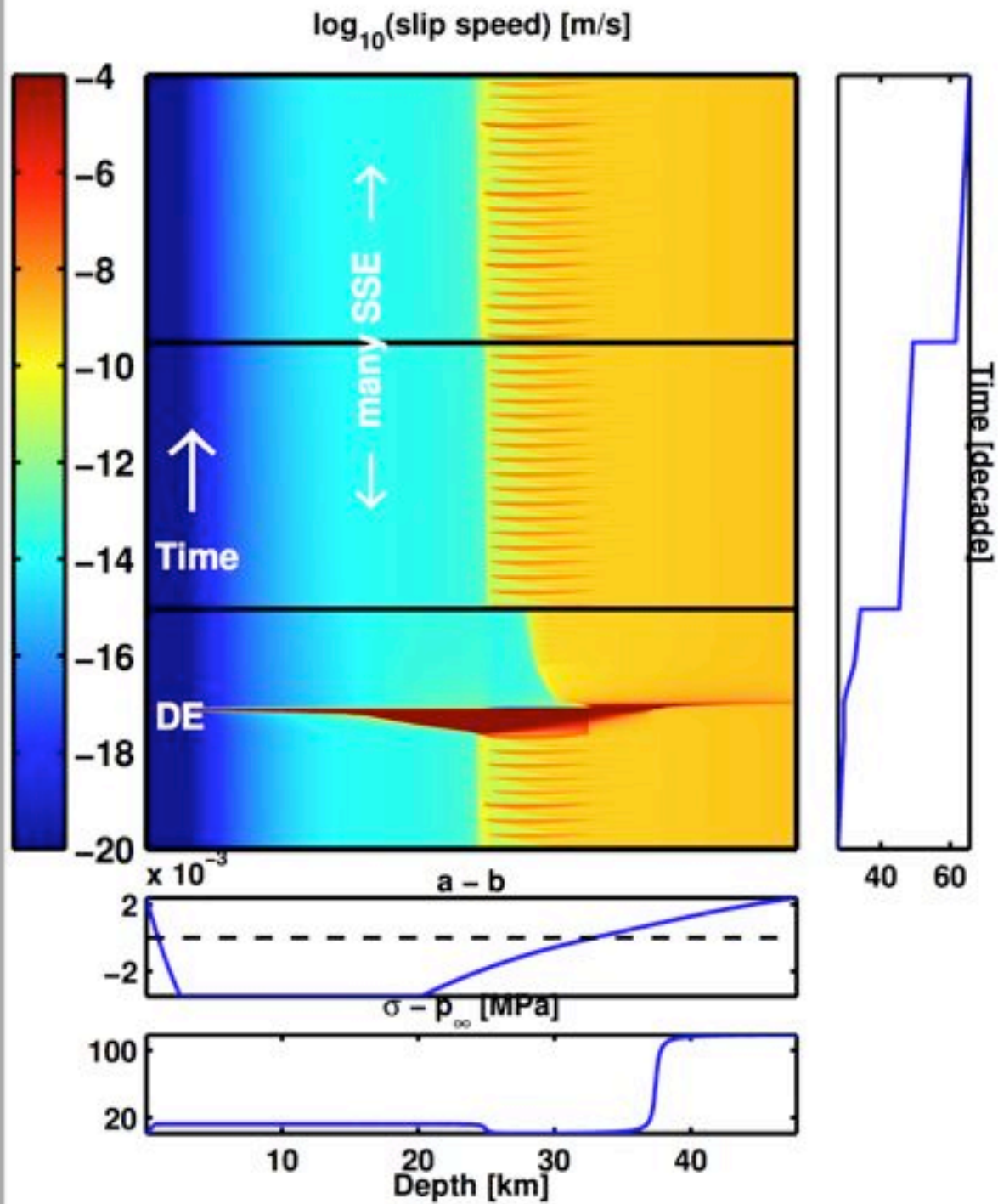
Inter-ETS propagation



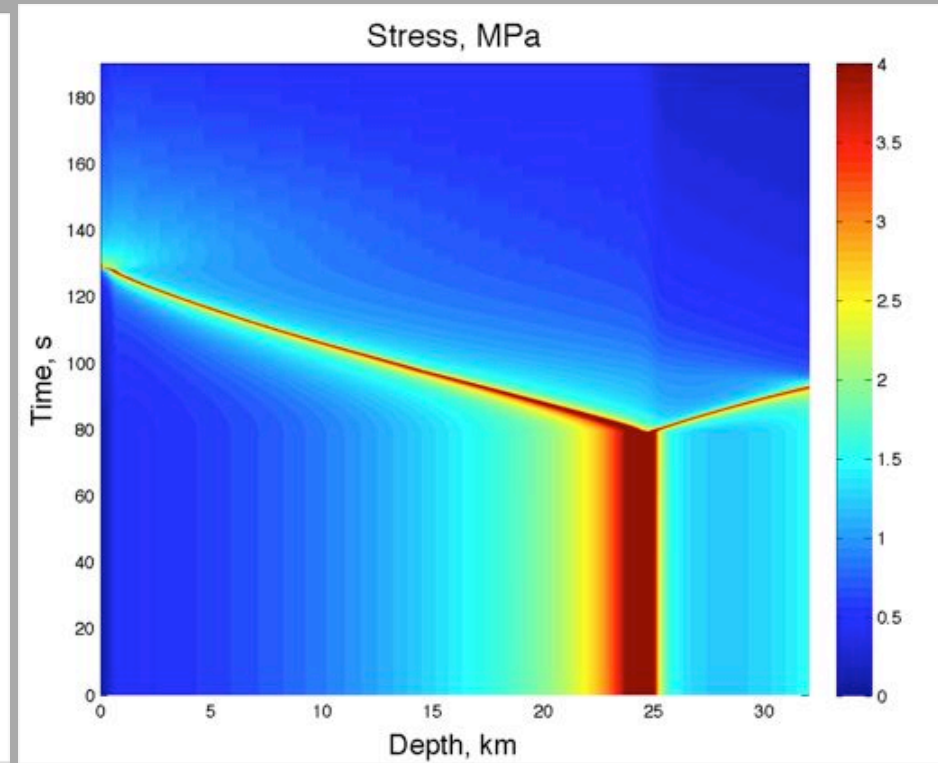
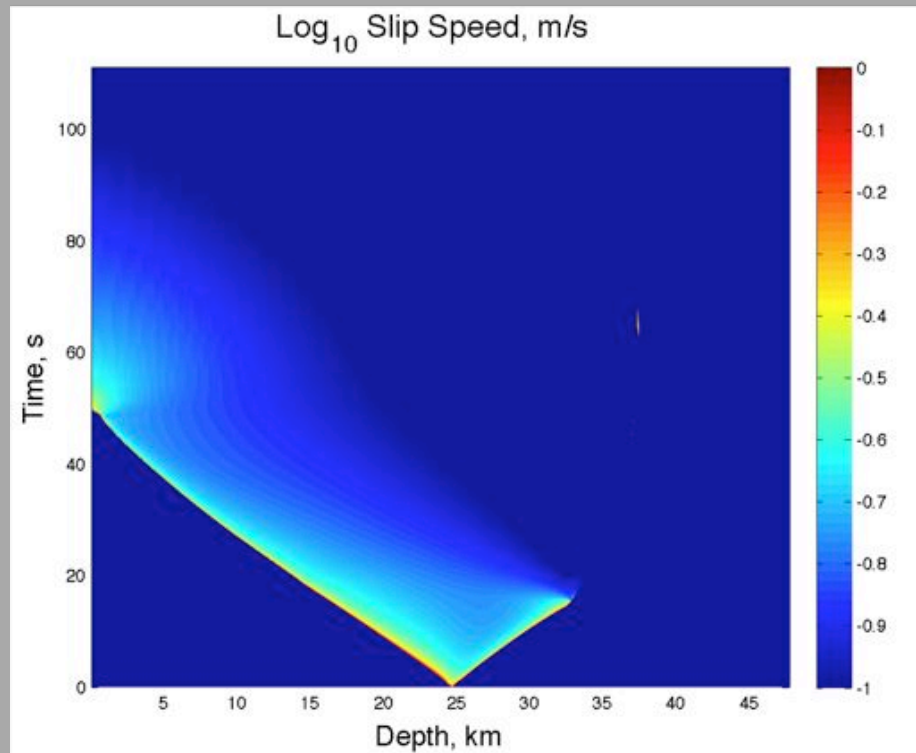
Inter-ETS phase may be reflected in tremor and may be detectable in inter-event GPS velocities

For sufficiently wide low stress zones, SSE ultimately nucleate dynamic events

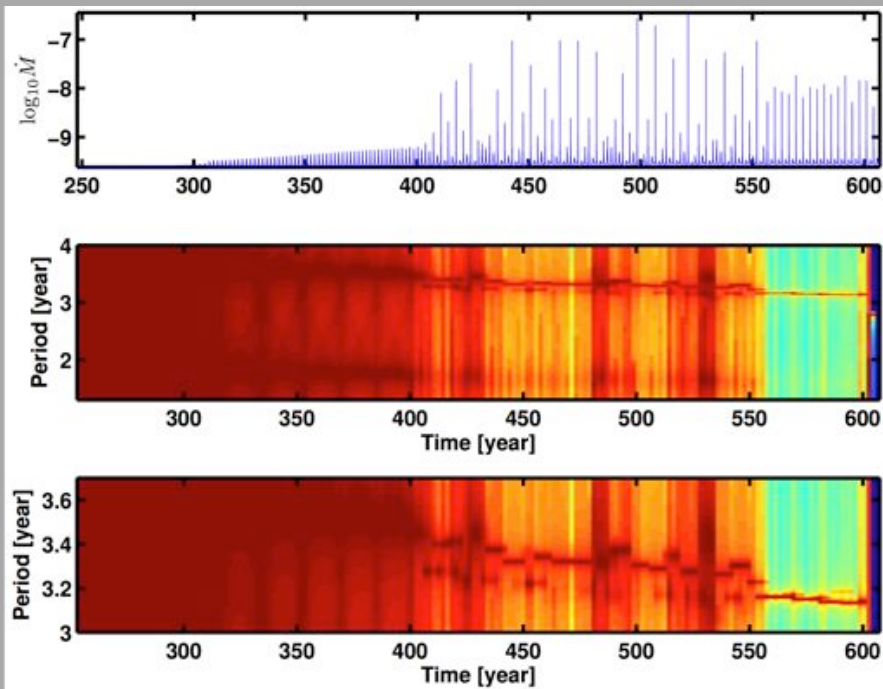




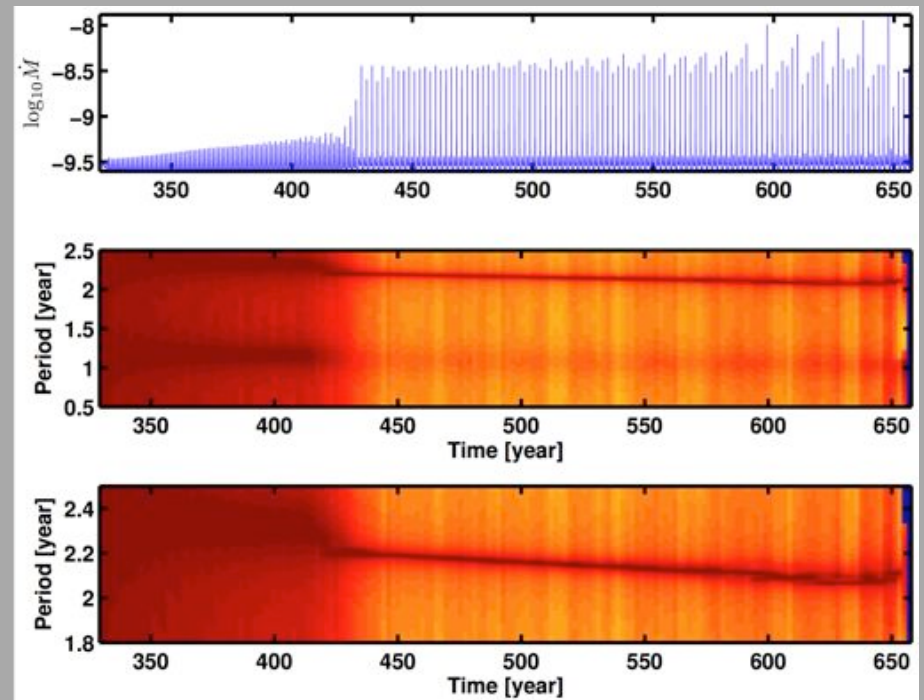
Dynamic Event Nucleates at Edge of ETS zone



SSE Repeat Period



Nominal Case

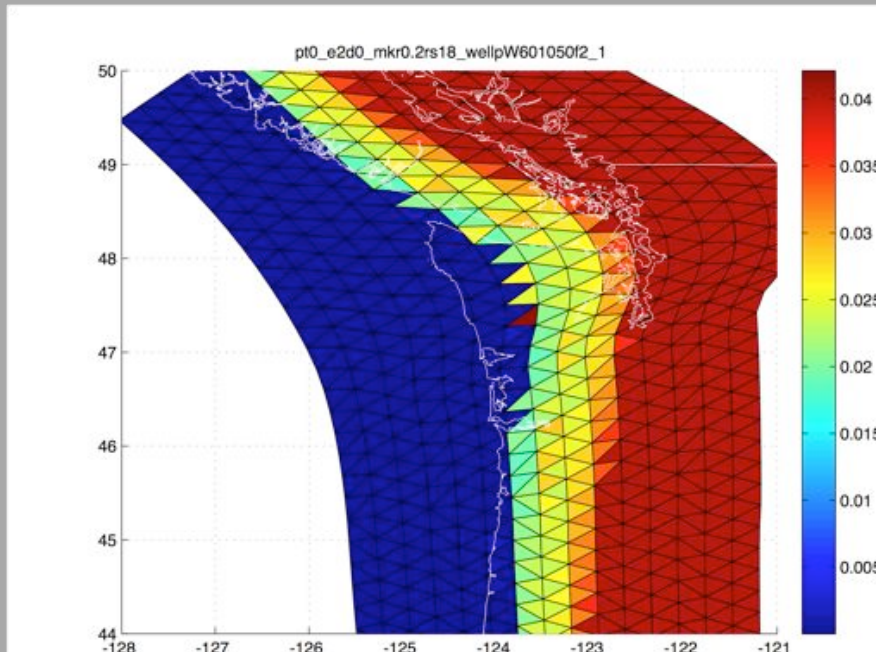


Decrease d_c by 2x

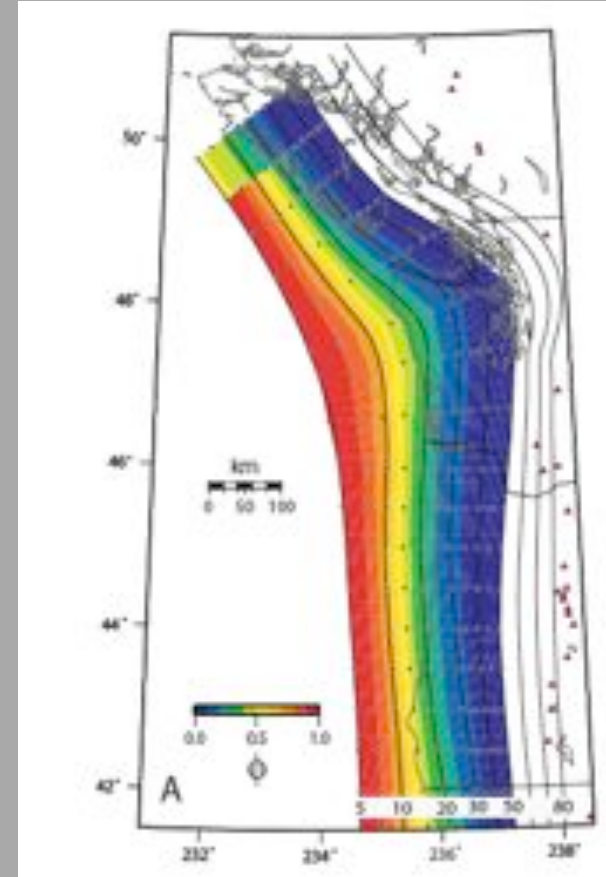
From linearized analysis of single-degree of freedom system:

$$T \approx 2\pi \left(\frac{d_c}{v^\infty} \right) \sqrt{\frac{a}{b-a}} \left[1 + \frac{f_0 E_p}{2\sqrt{2}b} F(a/b) \right] G(W/h^*)$$

Pseudo 3D Deformation Model: Inter-ETS sliprate

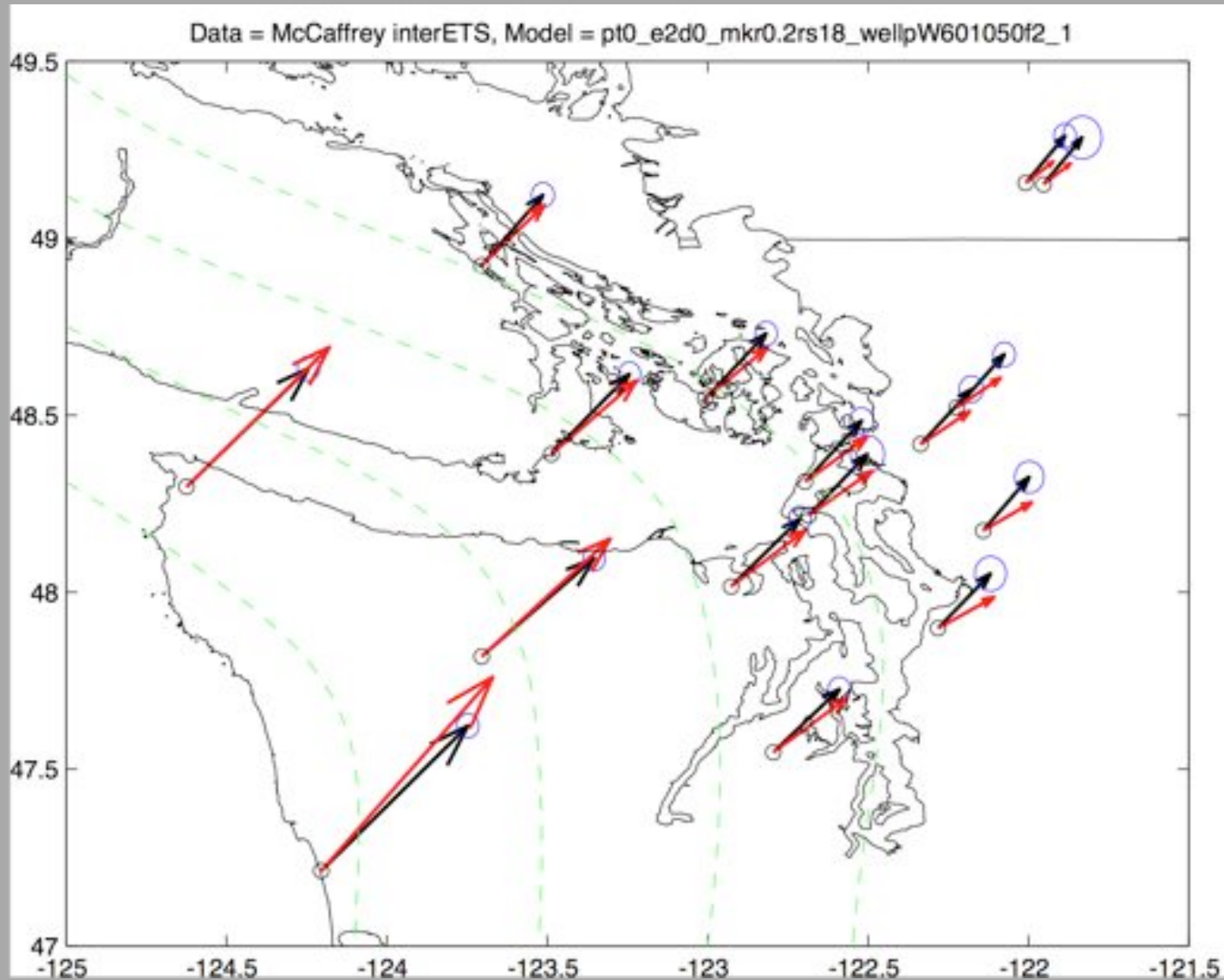


Slip speed a function of depth only, as determined by 2D physical model.



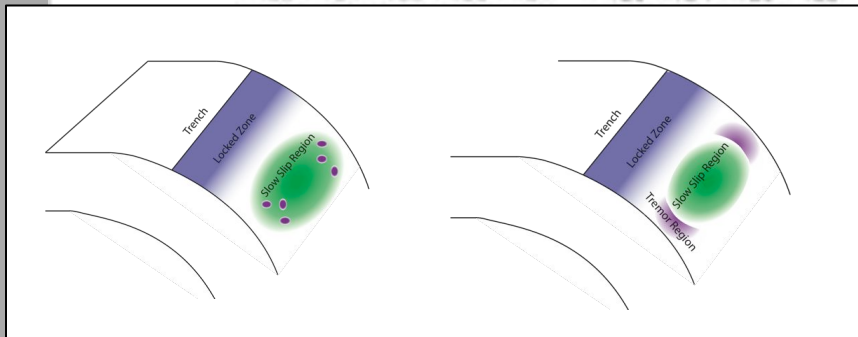
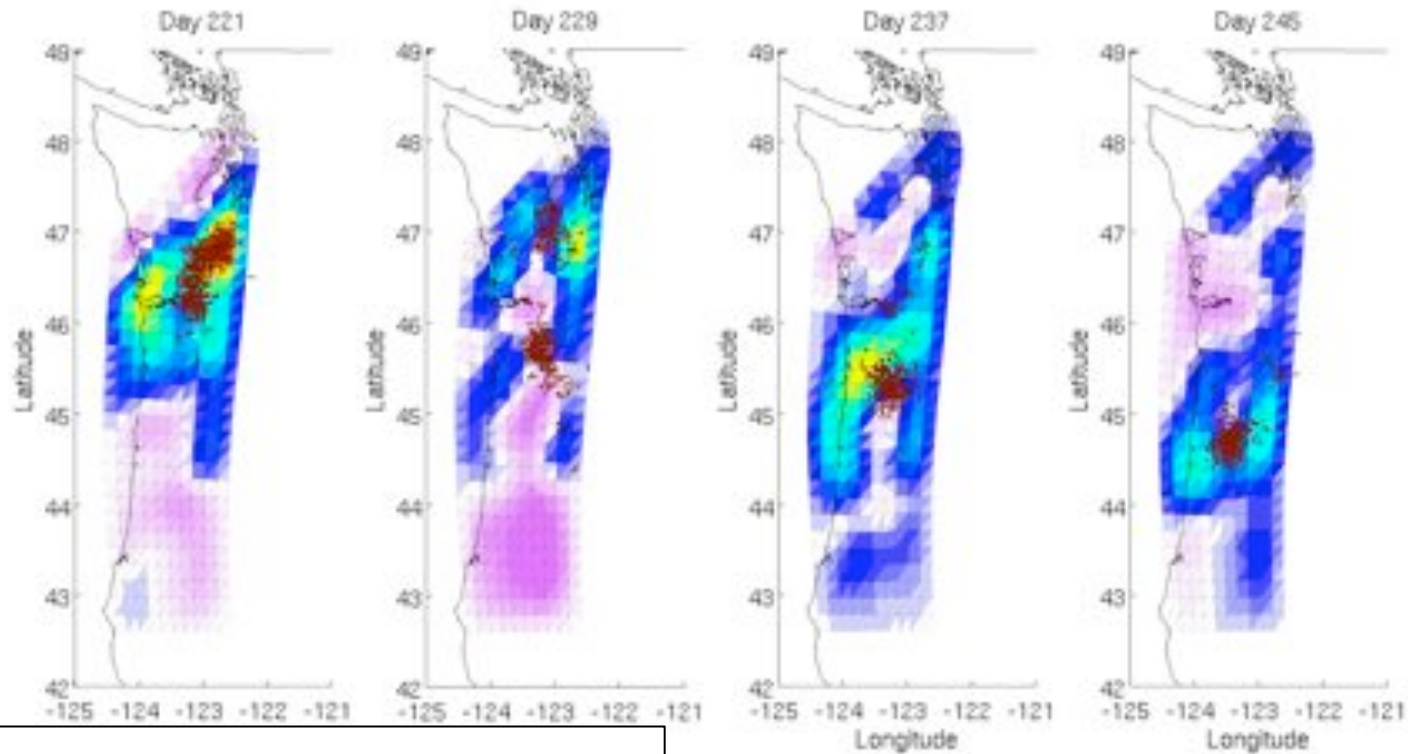
McCaffrey et al, 2007, inversion

Pseudo-3D Fit to Inter-ETS Deformation



'Data' courtesy R. McCaffery

Space-Time Relationship between Slow-Slip and Tremor



Bartlow, Miyazaki, and Segall,
this meeting.

Low Frequency Earthquakes

LFE moment: $M_0 \sim 3 \times 10^{11}$ N-m, [Ide, 2007]

Duration: $T \sim 0.3$ s, [Ide, 2007; Shelly et al, 2007]

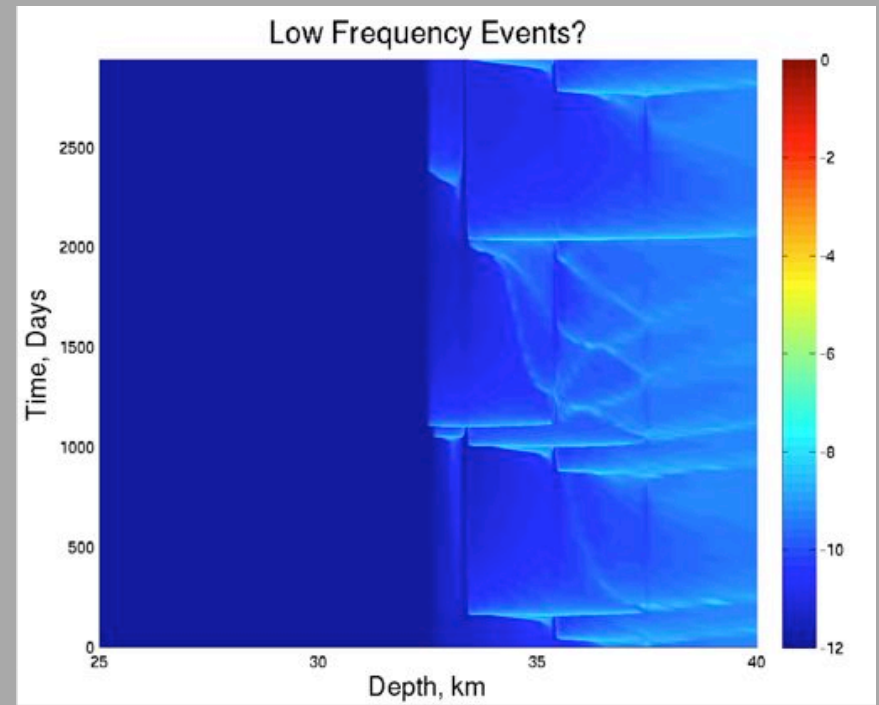
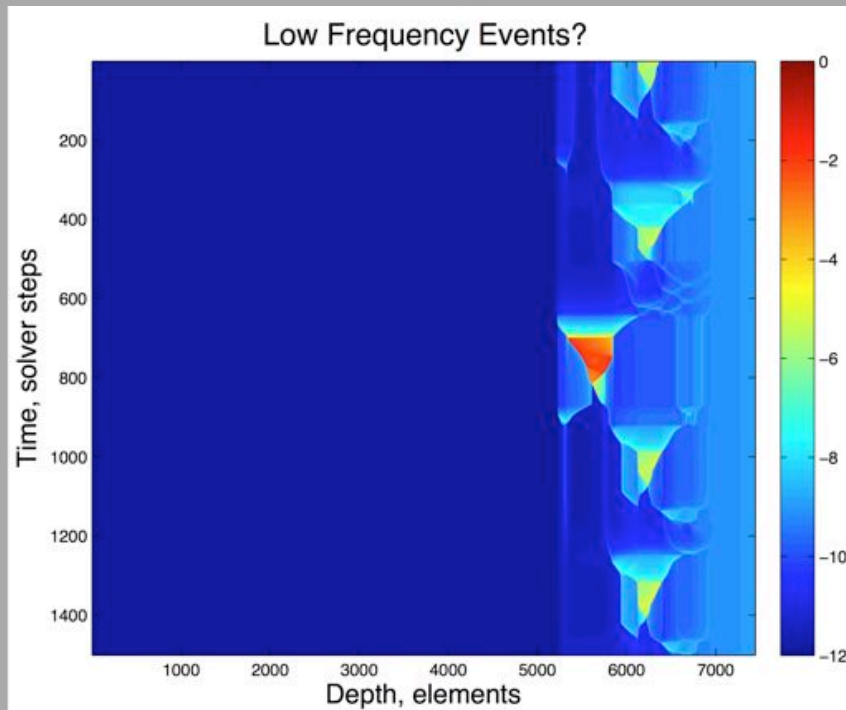
Moment rate: $\dot{M}_0 \sim 10^{12}$ N-m/s.

Challenge: Small areas of the plate interface must accelerate to slip-speeds sufficient to radiate seismic waves, without dynamic rupture continuing outside the LFE source region.

Hypothesis: Local regions of high permeability, perhaps due to fractures, allow rapid drainage and fast slip. Stressed by slow-slip in the surrounding regions.

Question: Is dilatancy sufficient to quench the instability, when ruptures reach the low-permeability, low effective stress surroundings? Or does thermal pressurization promote runaway dynamic rupture?

Test: Local regions w/ infinite diffusivity



Chen, Bradley, Segall

Local areas of high slip-speed decelerate after encountering low permeability background.

Conclusions

- Dilatancy allows slip to nucleate at low speeds but can limit fast slip.
- High pore-pressure mitigates against frictional and thermal weakening, thus favoring slow slip (consistent with seismological observations).
- For plausible material parameters, the predicted depth range, moment-rate, and repeat period are comparable to observations.
- Slow-slip behavior occurs for a broad range of parameters.
- Behavior highly dependent on depth dependent effective stress, as well as frictional properties.

Implications/Future Work

- For large part of parameter space, a slower phase is observed: Implication for inter-ETS tremor/slip? Need 3D models.
- For simple parameter distributions, transition between locked and steady slip at plate-velocity changes through seismic cycle: Implications for geodetic observations.
- Simple models exhibit variable behavior throughout seismic cycle. Slow-slip events penetrate into locked zone?

Implications/Future Work

- Slow slip may evolve into dynamic rupture. Diagnostic behavior prior to dynamic event?
- For simple distributions of material properties, slip in the ETS zone lags plate-rate. Consistent with geodetic observations?
- Coseismic (or rapid postseismic?) rupture into ETS zone? Implications for seismic hazard. Models with finite thickness shear zones (coming) will reduce the coseismic stress drop.
- Fractures within the ETS zone allow rapid drainage and may provide a mechanisms for LFEs.